

A NEUROFUZZY TECHNIQUE TO PREDICT SEISMIC LIQUEFACTION POTENTIAL OF SOILS

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Abstract: Liquefaction potential is a scientific assessment parameter to assess liquefaction of medium to fine grained cohesion-less soil due to earthquake shaking. In this paper alternative liquefaction potential prediction models have been developed using adaptive neuro fuzzy inference system (ANFIS) and multiple linear regression (MLR) technique. Geological survey of the study area was performed and forty locations were identified to perform standard penetration test (SPT). Disturbed and undisturbed soil samples were collected from the borehole to execute the laboratory tests. The bore-log datasets were used for determining liquefaction potential of the cohesion-less soils. The analytical approach by Idriss and Boulanger (I & B) has been applied initially to estimate liquefaction potential of soil on the basis of standard penetration test datasets obtained from the field investigations. To develop the ANFIS models 101 datasets were collected and incorporated for the development of fuzzy neural network models. Multiple linear regression (MLR) models have also been developed and the results were compared with neuro-fuzzy models. Based on obtained results it can be stated that the developed adaptive neuro fuzzy inference system models have better prediction ability to predict liquefaction potential with satisfactory level of confidence and can be used as an alternative tool.

Key words: *Liquefaction potential, ANFIS, standard penetration test, Idriss and Boulanger multiple linear regression*

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1. Introduction

On 26th January 2001, an earthquake originated in Bhuj (India) with maximum horizontal acceleration 0.35 g, damaged many medium and high rise buildings in and around Bhuj city [1]. The city buildings experienced differential settlement by violent shaking; this phenomenon was due to liquefaction which is caused by earthquake. Soil liquefaction occurs in loose, saturated cohesion-less soil units (sands

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and silts) and sensitive clays. Different methods like modified Seed's method, Tokimatsu and Yoshimi method and Idriss and Boulanger method etc. are used to estimate liquefaction potential using soil properties and seismic parameters. Soil properties are determined using in situ SPT and laboratory testing. However, in-situ testing is tedious method involving skilled labour, high cost and extra time. Therefore, alternative approach with economical and reliable prediction of liquefaction has been executed considering the soft computing and multi linear regression approach.

Though soft computing methods have been applied in various field of civil engineering however limited applications are available in the area of assessment of liquefaction potential using ANFIS. Some researchers like Goh, 1995, 2002; Wang et al., 2010; Moradi et al., 2011; Wang and Rahman, 1999; Hanna et al., 2007a, 2007b; Hsu et al. 2006; kayabah, 1996; Sitharam, et al., 2004; Rao et al., 2007; Chiru-Danger et al. 2001; Juang et al. 2000, 2001; Hsu et al. 2006; Ramakrishnan et al., 2008; Gracia et al., 2008; kayadelen et al., 2009 etc. [4–13, 1, 14–17] have developed the models using neural network technique for assessing liquefaction potential.

Fuzzy neural network which is integration of well-known fuzzy and neural network technique has been applied for the assessment of liquefaction potential in this work. Fuzzy neural network which was first proposed by Jang [2] in fuzzy modeling environment is divided into two areas: linguistic fuzzy modeling which is focused on interpretability is mainly the Mamdani model [3]; and precise fuzzy modeling that is focused on accuracy is mainly the Takagi-Sugeno-Kang (TSK) model. Adaptive Neuro-Fuzzy Inference System (ANFIS) falls in the category of precise fuzzy modeling.

Current research is the effort of assessing liquefaction potential of Allahabad city situated near the banks of river Ganga and Yamuna. Since alluvial soil is abundantly present in this vicinity and soil strata on the bank of river are mainly consist of sand, silt and clay soil at various depths. The upper part of strata contains major portion of silty soil and sandy silt enhancing probability of liquefaction. So there is a major chance of liquefaction occurrence in the upper soil strata during the earthquake. Analytical method given by Idriss and Boulanger (I & B) was used initially for liquefaction potential assessment, later on it was incorporated in Neuro-fuzzy and MLR modeling approach for predicting liquefaction potential of soils.

2. Liquefaction Potential Assessment

2.1 Idriss and Boulanger's method

Geotechnical professionals generally investigate subsurface to evaluate the potential for liquefaction. The most common techniques using standard penetration test (SPT) i.e. blow count (commonly referred as to the "N-value"). The liquefaction potential assessment by analytical approach follows certain protocols:

1. Estimation of the cyclic stress ratio (CSR) induced at various depths within the soil by the earthquake.

2. Estimation of the cyclic resistance ratio (CRR) of the soil, i.e. the cyclic shear stress ratio which is required to cause initial liquefaction of the soil.
3. Evaluation of factor of safety against liquefaction potential of in situ soils

Calculation of CSR: Modus operandi by Idriss & Boulanger [18] for evaluation of CSR is same as “simplified method”. Right after CSR calculated from the equation (1).

$$CSR = \tau_{avg} / \sigma'_v = 0.65 (a_{max} / g) (\sigma_v / \sigma'_v) r_d \quad (1)$$

Value of CSR is adjusted for the moment magnitude $M = 7.5$. Accordingly the value of CSR is given as

$$(CSR)_{M=7.5} = CSR / MSF = 0.65 (\sigma_v a_{max} / \sigma'_v) \frac{r_d}{MSF} \quad (2)$$

A new parameter r_d which could be adequately expressed as a function of depth and earthquake magnitude (M) was introduced and can be explain from following relations:

$$\ln(r_d) = \alpha(z) + \beta(z)M \quad (3)$$

$$\alpha(z) = -1.012 - 1.126 \sin(z/11.73 + 5.133) \quad (4a)$$

$$\beta(z) = 0.106 + 0.118 \sin(z/11.28 + 5.142) \quad (4b)$$

where z is the depth in meters and M is moment magnitude. These equations were appropriated for depth $z \leq 34$ m however for depth $z > 34$ m; the following expression can be used:

$$r_d = 0.12 \exp(0.22M) \quad (5)$$

$CSR_{7.5}$ is the cyclic stress ratio for magnitude of 7.5 earthquakes, magnitude smaller or larger than 7.5, introduces a correction factor namely magnitude scaling factor MSF defined by the following equation given by [19]:

$$MSF = 10^{2.24} / M^{2.56} \quad (6)$$

Calculation of CRR: Idriss and Boulanger [18] adjusted the equation of CRR for clean sands as follows

$$CRR = \exp \left\{ \frac{(N_1)_{60cs}}{14.1} + \left(\frac{(N_1)_{60cs}}{126} \right)^2 - \left(\frac{(N_1)_{60cs}}{23.6} \right)^3 + \left(\frac{(N_1)_{60cs}}{25.4} \right)^4 - 2.8 \right\} \quad (7)$$

Subsequent expressions describes the way parameters in the above equation is calculated

$$(N_1)_{60cs} = (N_1)_{60} + (\Delta N_1)_{60} \quad (8a)$$

$$(\Delta N_1)_{60} = \exp(1.63 + 9.7/FC - (15.7/FC)) \quad (8b)$$

$$(N_1)_{60} = C_N (N)_{60} \quad (8c)$$

The use of equations in preceding articles provides a convenient means for evaluating the cyclic stress ratio required to cause liquefaction for cohesion-less soils with varying fines content.

Calculation of Factor of Safety: If the cyclic stress ratio caused by an earthquake is greater than the cyclic resistance ratio of the in situ soil, then liquefaction could occur during the earthquake, and vice versa. The factor of safety (FOS) against liquefaction is defined as:

$$FS_{\text{Liquefaction}} = \text{CRR}/\text{CSR} \tag{9}$$

Liquefaction is predicted to occur when $FS \leq 1.0$, and liquefaction predicted not to occur when $FS > 1$. The higher the factor of safety, the more resistant against liquefaction [20], however, soil that has a factor of safety slightly higher than 1.0 partially liquefy during the earthquake.

2.2 Adaptive Neuro-Fuzzy Inference System (ANFIS)

Adaptive Neuro-Fuzzy Inference System (ANFIS) is one of the most successful schemes which combine the benefits of ANN and FIS into a single capsule [1]. The attractive features of an ANFIS include: easy to implement, fast and accurate learning, strong generalization abilities, excellent explanation facilities through fuzzy rules, and easy to incorporate both linguistic and numeric knowledge for problem solving [21, 22]. According to the neuro-fuzzy approach, a neural network is proposed to implement the fuzzy system. A typical architecture of an ANFIS, in which a circle indicates a fixed node, whereas a square indicates an adaptive node, is shown in Fig. 1. In this structure, there are input and output nodes, and in the hidden layers, there are nodes functioning as membership functions (MFs) and rules. For simplicity, we assume that the examined FIS has two inputs and one output. For a first-order Sugeno fuzzy model [3], a classic rule set with two fuzzy “if then” rules is as following:

$$\text{Rule 1: if } a \text{ is } A_1 \text{ and } b \text{ is } B_1, \text{ then } f_1 = p_1a + q_1b + r_1, \tag{10a}$$

$$\text{Rule 2: if } a \text{ is } A_2 \text{ and } b \text{ is } B_2, \text{ then } f_2 = p_2a + q_2b + r_2. \tag{10b}$$

where a and b are the two crisp inputs, and A_i and B_i are the linguistic labels associated with the node function.

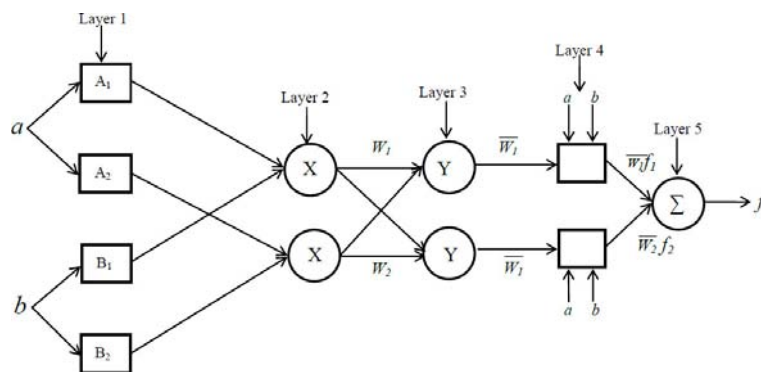


Fig. 1 First order Sugeno ANFIS architecture.

As indicated in Fig. 1, the system has a total of five layers. The functioning of each layer is described as follows [1].

Input node (Layer 1): Nodes in this layer contains membership functions. Parameters in this layer are referred to as premise parameters. Every node i in this layer is a square and adaptive node with a node function:

$$O_i^1 = \mu_{A_i}(a) \text{ for } i = 1, 2. \quad (11)$$

where x is the input to node i , and A_i is the linguistic label (small, large, etc.) associated with this node function. In other words, O_i^1 is the membership function of A_i and it specifies the degree to which the given x satisfies the quantifier A_i .

Rule nodes (Layer 2): Every node in this layer is fixed node labeled X, whose output is product of all incoming signals.

$$O_i^2 = w_i = \mu_{A_i}(a) \times \mu_{B_i}(b) \text{ for } i = 1, 2 \quad (12)$$

Average nodes (Layer 3): Every node in this layer is fixed node labeled Y. The i^{th} node calculates the ratio between the i^{th} rule's firing strength to the sum of all rule's firing strengths. Every node of these layers calculates the weight, which is normalized. For convenience, outputs of this layer are called normalized firing strengths.

$$O_i^3 = \bar{w}_i = \frac{w_i}{w_1 + w_2} \text{ for } i = 1, 2 \quad (13)$$

Consequent nodes (Layer 4): Every node i in this layer is an adaptive node with a node function

$$O_i^4 = \bar{w}_i \times f_1 = \bar{w}_i \times (p_i a + q_i b + r_i) \quad (14)$$

Where \bar{w}_i is a normalized firing strength from layer 3 and (p_i, q_i, r_i) is the parameters set of this node. Parameters in this layer are referred to as consequent parameters.

Output node (Layer 5): The single node in this layer is a fixed node labeled \sum , which computes the overall output as the summation of all incoming signals:

$$\text{Overall output} = O_i^5 = \sum_i \bar{w}_i \times f_1 = \frac{\sum_i w_i \times f_i}{\sum_i w_i} \quad (15)$$

2.3 Multiple Linear Regression (MLR) Analysis

Regression analysis is the study of establishing the functional relation between independent and dependent variables. The independent variables may vary from one or greater than one depending on the requirement of the dependent models. However, the number of dependent variables is strictly restricted to one. The general formula of regression establishing relationship between different independent variables and a dependent variable is shown below [23]:

$$y = b_0 + b_1 x_1 + b_2 x_2 + \dots b_p x_p \quad (16)$$

$$\text{or, } y = b_0 + \sum b_i x_i \quad (17)$$

where, $i = 1, 2, \dots, p$

y is the dependent variable (liquefaction potential in this case)

$x_1, x_2 - x_p$ are independent variables,

and $b_0, b_1, b_2 - b_p$ are the coefficients that has to be determined using regression analysis.

3. Methodology

After geological survey, soil investigation of the sites and its surroundings were carried out initially for pertinent data collection. In-situ standard penetration test was conducted to collect disturbed and undisturbed soil samples from the 40 boreholes. The required soil properties were investigated in the laboratory to determine liquefaction potential of cohesion-less soils using I & B analytical approach. The bore-log charts of different boreholes were used to collect the input datasets whereas output datasets were obtained from I & B analytical method. To develop the ANFIS and MLR models 101 datasets were collected in terms of input and output values of the models.

3.1 Experimental method

Standard penetration test was conducted in order to collect disturbed and undisturbed soil samples. Disturbed and undisturbed soil samples were collected from these boreholes up to the depth of 10 meters. The SPT N-value was also determined at a regular interval of 1.5 m depth [24]. Disturbed soil samples were used to determine liquid limit; plastic limit; angle of internal friction; particle size finer than 2 mm, 0.075 mm and 0.002 mm and undisturbed samples were used to determine natural water content [25-27], bulk unit weight. All experiments were conducted according to bureau of Indian standard's guidelines for soil testing.

Data modification: Corrected SPT-N values are required to estimate liquefaction potential using I & B method hence standard procedure for correcting SPT-N value was adopted as per the Indian Standard IS: 2131-1981 [24]. A brief discussion on corrected SPT-N value is discussed hereunder:

Correction for overburden pressure: N-value obtained from SPT test is corrected first which is either calculated by the equation:

$$N_1 = C_N \quad (18)$$

C_N is correction factor obtained directly from the graph given in Indian Standard Code (IS: 3121-1981) (Fig. 2).

It can also be calculate from the following relationship i.e.

$$C_N = 0.77 \log_{10} \frac{2000}{p} \quad (19)$$

where, p is effective overburden pressure in kN/m^2 [28].



Fig. 2 Correction due to overburden pressure.

Dilatancy Correction: The values obtained in overburden pressure (N_1) shall be corrected for dilatancy if the stratum consist of fine sand and silt below water table for the values of N_1 greater than 15 by following equation [29]:

$$N_c = 15 + 0.5(N_1 - 15) \quad (20)$$

The range of soil properties found through SPT and other laboratory test used as input vectors in ANFIS method is shown in Tab. I. Two parameters i.e. water table (W) and earthquake magnitude (M) were varied for parametric studies. Level of water table varied from 0, 2, 4, 6 and 8 m from ground surface and earthquake magnitude varied for 6.0, 7.0 and 8.0. Hence, 15 combinations were formed for calculating CSR value by I & B method for the specific depth of water table and earthquake magnitude as shown in Tab. II. Similarly, CSR values were obtained for different combination of depth and earthquake magnitude.

| Input Parameters | Ranges |
|----------------------------------|-------------|
| depth (m) | 0-10 |
| SPT-N value | 0-50 |
| Bulk unit weight (γ_t) | 1.31-2.36 |
| Particle finer than 0.075 mm (%) | 18.34-99.64 |
| Natural water content | 1.16-32.3 |

Tab. I Ranges of Input Parameters.

| | | | | | |
|--------------------------------------|-----|-----|-----|---|---|
| Depth of water table (m) | 0 | 2 | 4 | 6 | 8 |
| Earthquake magnitude (Richter scale) | 6.0 | 7.0 | 8.0 | — | — |

Tab. II Assumed Water Table and Earthquake Magnitude.

4. Development of ANFIS and MLR Models

Since this study is based on SPT and bore log chart datasets. Initially two fundamental input variables i.e. depth (z) and SPT-N value (N) were chosen for the development of the fuzzy neural network models for predicting liquefaction potential. Subsequently input variables were increased to develop an optimum liquefaction potential model with minimum error. Study carried out up to five input variables comprising depth (d), SPT-N value (N), bulk density (ρ_f), particle size finer than 0.075 mm (D_x) and natural/field moisture content (w_f). In this, 30 borehole datasets were used for training and testing whereas 10 borehole datasets were reserved for validating the fuzzy neural network models. Normalized datasets were used for models using following equation [30].

$$\alpha = \frac{\alpha_{actual} - \alpha_{min.}}{\alpha_{max.} - \alpha_{min.}} \quad (21)$$

where, α = Normalized value.
 α_{actual} = data which has to be normalized, the input and output parameter's value.
 α_{min} = minimum value of data.
 and, α_{max} = maximum value of data.

ANFIS modeling tool was used for all operations in which networks were trained for varying numbers of epochs. Grid partitioning method and triangular membership function were used to generate fuzzy inference system from input variables, whereas linear membership function was used for target variable. Hybrid optimization technique was used for training FIS [31]. Inputs were increased gradually to study the effect of individual parameter on liquefaction. Output parameter (that is occurrence of liquefaction) in the ANFIS model is designed to answer in like/unlike format based on I & B method [32].

To identify different network architecture with its fundamental attributes a coding method was used for different networks, as such $W_X M_Y$ where, W_X denotes depth of water table and M_Y is earthquake magnitude value. The predicted values of liquefaction potential by developed models are discussed in subsequent heading.

Regression analyses were also carried out to establish the functional relation between independent and dependent variables to develop MLR models. The developed multivariate liner equations from MLR analysis are presented in Tab. VIII. These equations are shown for all fifteen combinations of water table and earthquake magnitude. The generalized form of MLR equations to predict liquefaction potential (LP) is as follows

$$LP = A_1 - A_2d + A_3N + A_4D_x + A_5w_f - A_6\rho_f \quad (22)$$

where, A_1 to A_6 represents the constant of the equation with the adopted variables i.e. depth (d), SPT-N value (N), percentage finer then 0.075 (D_x), moisture content (w_f) and bulk density (ρ_f).

5. Results and Discussion

The developed ANFIS and MLR models were validated using reserve datasets. As mentioned above five levels of water table and three earthquake magnitudes were considered for assessing liquefaction potential using I & B, ANFIS and MLR technique. These parameters resulted in total of fifteen set of liquefaction values. Tab. III(a), IV(a) and V(a) show liquefaction potential values for these combinations predicted by ANFIS models. Using the same datasets MLR models were developed, validated and compared with observed values obtained by conventional methods are depicted in Tab. III(b), IV(b) and V(b).

Tab. III to V displays the results of liquefaction potential on the basis of CRR/CSR obtained from I & B method where as ANFIS and MLR models predictions are based on five input parameters. In some of the combinations, the liquefaction potential values predicted by ANFIS and MLR models is not in accordance with I & B method. The comparison between the predicted values of optimum ANFIS models and I & B method are also shown in Figs. 3 to 5. This study also highlights the drawbacks with respect to predicted value by ANFIS method are as follows: W_6M_2 ANFIS model is giving liquefaction potential as 0.952 instead of 1.25; similarly W_6M_4 model predicting 1.109 compared to 0.826. In case of W_6M_6 model it is 1.027 and 1.25 compared to 1.00 and 0.995 similarly in W_6M_8 it is 1.25, 1.25, 1.024 and 1.25 in comparison to 0.942, 0.874, 0.918 and 0.815 as displayed in Tab. III(a). In Tab. IV(a) liquefaction potential is predicted by ANFIS model for W_7M_{24} is 0.993 compared to 1.037. In case of Tab. V(a) liquefaction potential predicted by ANFIS model for W_8M_8 is 1.001 and 1.25 in comparison to 0.884 and 0.956. Similarly MLR also predicted some results incorrectly for example model M_6W_0 gave four incorrect prediction as 1.129, 1.154, 1.312, & 1.154, model M_6W_2 gave five incorrect prediction as 1.799, 1.224 & 1.749, 1.749 & 1.749 model M_6W_4 gave six incorrect prediction as 1.010, 1.539, 2.113, 2.113, 1.800 & 2.113 model M_6W_6 also gave six incorrect prediction as 0.000, 2.134, 2.134, 1.808, 2.134 & 0.829 and model M_6W_8 gave five incorrect prediction as 0.000, 2.025, 2.025, 1.719, 2.025. Above incorrect predictions were found for earthquake magnitude of 6.0. The details of predicted value for earthquake magnitude of seven and eight respectively may also viewed in Tab. IV(b) & V(b) to observe the limitations of these methods.

The results obtained from lesser input vectors were ignored since liquefaction values obtained with the combination of five input vectors were close to I & B method. Coefficient of determination (COD or R^2), mean absolute error (MAE) and root mean square error (RMSE) obtained for fifteen cases by ANFIS and MLR models are summarized in Tab. VI. The coefficient of determination is as high as 0.998 for the earthquake magnitude 7.0 whereas water table is at ground level for ANFIS models. As per the results, most of the ANFIS models have coefficient of determination greater than 0.9 which illustrate good prediction capabilities of ANFIS models. The ANFIS models from combinations M_6W_0 , M_7W_0 and M_8W_6 having the coefficient of determination values of 0.9943, 0.9979 and 0.9922 respectively, that illustrate that ANFIS models needs improvement with a lot of datasets. However, the incorrect predicted liquefaction potential from these models varied from one to four (bolded results in respective Table) out of total 30 validation

| S. No. | Depth (z) | SPT-N value | For network Mw ₆ | | | For network Mw ₇ | | | For network Mw ₈ | | | For network Mw ₉ | | | For network Mw ₆ | | | For network Mw ₇ | | | | |
|--------|-----------|-------------|-----------------------------|----------------------|-------|-----------------------------|-----------------------------|----------------------|-----------------------------|--------|-----------------------------|-----------------------------|-------|--------|-----------------------------|----------------------|-------|-----------------------------|-----------------------------|----------------------|-------|--------|
| | | | lique. Pot. by I & B method | lique. Pot. by ANFIS | ratio | status | lique. Pot. by I & B method | lique. Pot. by ANFIS | ratio | status | lique. Pot. by I & B method | lique. Pot. by ANFIS | ratio | status | lique. Pot. by I & B method | lique. Pot. by ANFIS | ratio | status | lique. Pot. by I & B method | lique. Pot. by ANFIS | ratio | status |
| 1 | 4.5 | 22 | 0.618 | Like | 0.618 | Like | 0.895 | Like | 1.172 | Unlike | 1.172 | Unlike | 1.241 | Unlike | 1.241 | Unlike | 1.241 | Unlike | 1.127 | Unlike | 1.241 | Unlike |
| 2 | 6 | 21 | 0.569 | Like | 0.576 | Like | 0.755 | Like | 0.941 | Like | 0.954 | Like | 1.127 | Unlike | 1.127 | Unlike | 1.127 | Unlike | 1.127 | Unlike | 1.127 | Unlike |
| 3 | 7.5 | 20 | 0.615 | Like | 0.601 | Like | 0.753 | Like | 0.89 | Like | 0.919 | Like | 1.027 | Unlike | 1.027 | Unlike | 1.027 | Unlike | 1.027 | Unlike | 1.13 | Unlike |
| ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 15 | 3 | 28 | 0.957 | Like | 0.931 | Like | 1.25 | Unlike | 1.25 | Unlike | 1.123 | Unlike | 1.25 | Unlike | 1.25 | Unlike | 1.25 | Unlike | 1.25 | Unlike | 1.25 | Unlike |
| ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 18 | 3 | 27 | 1.06 | Unlike | 1.023 | Unlike | 1.25 | Unlike | 1.25 | Unlike | 1.092 | Unlike | 1.25 | Unlike | 1.25 | Unlike | 1.25 | Unlike | 1.25 | Unlike | 1.25 | Unlike |
| ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 25 | 9 | 14 | 0.469 | Like | 0.432 | Like | 0.58 | Like | 0.692 | Like | 0.549 | Like | 0.803 | Like | 0.803 | Like | 0.803 | Like | 0.803 | Like | 0.914 | Like |
| ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 30 | 7.5 | 17 | 0.505 | Like | 0.452 | Like | 0.648 | Like | 0.791 | Like | 0.657 | Like | 0.934 | Like | 0.934 | Like | 0.934 | Like | 0.934 | Like | 1.042 | Unlike |
| ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 34 | 7.5 | 28 | 0.746 | Like | 0.688 | Like | 0.928 | Like | 1.109 | Unlike | 0.826 | Like | 1.25 | Unlike | 1.25 | Unlike | 1.25 | Unlike | 1.25 | Unlike | 1.25 | Unlike |

Tab. III(a) Liquefaction potential from ANFIS model for earthquake magnitude 6.0 with varying water level.

| S. No. | Depth (z) | SPT -N value | For network:MAW ₀ | | | | For network:MAW ₁ | | | | For network:MAW ₄ | | | | For network:MAW ₆ | | | | For network:MAW ₈ | | | |
|--------|-----------|--------------|------------------------------|--------|--------|--------|------------------------------|--------|--------|--------|------------------------------|--------|--------|--------|------------------------------|--------|--------|--------|------------------------------|--------|--------|-----|
| | | | lique. Pot. by I & B method | ratio | status | MLR | lique. Pot. by I & B method | ratio | status | MLR | lique. Pot. by I & B method | ratio | status | MLR | lique. Pot. by I & B method | ratio | status | MLR | lique. Pot. by I & B method | ratio | status | MLR |
| 1 | 4.5 | 22 | 0.618 | Like | 1.129 | Unlike | 1.799 | Unlike | 1.172 | Unlike | 2.229 | Unlike | 1.241 | Unlike | 2.418 | Unlike | 1.241 | Unlike | 2.423 | Unlike | | |
| 2 | 6 | 21 | 0.569 | Like | 0.660 | Like | 0.875 | Like | 0.941 | Like | 1.010 | Unlike | 1.127 | Unlike | 1.160 | Unlike | 1.127 | Unlike | 1.238 | Unlike | | |
| 3 | 7.5 | 20 | 0.615 | Like | 0.000 | Like | 0.753 | Like | 0.89 | Like | 0.000 | Like | 1.027 | Unlike | 0.000 | Like | 1.130 | Unlike | 0.000 | Like | | |
| 4 | 4.5 | 28 | 0.75 | Like | 1.154 | Unlike | 1.054 | Unlike | 1.703 | Unlike | 2.025 | Unlike | 1.434 | Unlike | 2.234 | Unlike | 1.434 | Unlike | 2.286 | Unlike | | |
| 5 | 6 | 45 | 1.556 | Unlike | 2.171 | Unlike | 2.029 | Unlike | 3.036 | Unlike | 3.819 | Unlike | 2.975 | Unlike | 4.304 | Unlike | 2.975 | Unlike | 4.437 | Unlike | | |
| 6 | 4.5 | 13 | 0.469 | Like | 0.458 | Like | 0.683 | Like | 0.791 | Like | 0.919 | Like | 0.951 | Like | 0.971 | Like | 0.951 | Like | 0.967 | Like | | |
| 7 | 6 | 21 | 0.562 | Like | 0.853 | Like | 0.755 | Like | 1.224 | Unlike | 1.539 | Unlike | 1.14 | Unlike | 1.729 | Unlike | 1.14 | Unlike | 1.783 | Unlike | | |
| 8 | 1.5 | 6 | 0.344 | Like | 0.824 | Like | 0.761 | Like | 1.749 | Unlike | 0.761 | Like | 0.761 | Like | 0.813 | Like | 0.761 | Like | 2.025 | Unlike | | |
| 9 | 6 | 12 | 0.394 | Like | 0.120 | Like | 0.533 | Like | 0.070 | Like | 0.000 | Like | 0.813 | Like | 0.042 | Like | 0.813 | Like | 0.123 | Like | | |
| 10 | 1.5 | 6 | 0.344 | Like | 0.824 | Like | 0.761 | Like | 1.749 | Unlike | 2.113 | Unlike | 0.761 | Like | 2.134 | Unlike | 0.761 | Like | 2.025 | Unlike | | |
| 11 | 3 | 28 | 0.957 | Like | 1.312 | Unlike | 1.83 | Unlike | 2.071 | Unlike | 2.449 | Unlike | 1.83 | Unlike | 2.642 | Unlike | 1.830 | Unlike | 2.656 | Unlike | | |
| 12 | 4.5 | 28 | 0.75 | Like | 1.154 | Unlike | 1.054 | Unlike | 1.703 | Unlike | 2.025 | Unlike | 1.434 | Unlike | 2.234 | Unlike | 1.434 | Unlike | 2.286 | Unlike | | |
| 13 | 6 | 45 | 1.556 | Unlike | 2.171 | Unlike | 2.029 | Unlike | 3.036 | Unlike | 3.819 | Unlike | 2.975 | Unlike | 4.304 | Unlike | 2.975 | Unlike | 4.437 | Unlike | | |
| 14 | 4.5 | 13 | 0.469 | Like | 0.458 | Like | 0.683 | Like | 0.791 | Like | 0.919 | Like | 0.951 | Like | 0.971 | Like | 0.951 | Like | 0.967 | Like | | |
| 15 | 6 | 21 | 0.562 | Like | 0.853 | Like | 0.755 | Like | 1.224 | Unlike | 1.539 | Unlike | 1.14 | Unlike | 1.729 | Unlike | 1.14 | Unlike | 1.783 | Unlike | | |
| 16 | 1.5 | 6 | 0.344 | Like | 0.824 | Like | 0.761 | Like | 1.749 | Unlike | 0.761 | Like | 0.761 | Like | 0.813 | Like | 0.761 | Like | 2.025 | Unlike | | |
| 17 | 6 | 12 | 0.394 | Like | 0.120 | Like | 0.533 | Like | 0.070 | Like | 0.000 | Like | 0.813 | Like | 0.042 | Like | 0.813 | Like | 0.123 | Like | | |
| 18 | 1.5 | 6 | 0.344 | Like | 0.824 | Like | 0.761 | Like | 1.749 | Unlike | 2.113 | Unlike | 0.761 | Like | 2.134 | Unlike | 0.761 | Like | 2.025 | Unlike | | |
| 19 | 3 | 28 | 0.957 | Like | 1.312 | Unlike | 1.83 | Unlike | 2.071 | Unlike | 2.449 | Unlike | 1.83 | Unlike | 2.642 | Unlike | 1.830 | Unlike | 2.656 | Unlike | | |
| 20 | 4.5 | 28 | 0.75 | Like | 1.154 | Unlike | 1.054 | Unlike | 1.703 | Unlike | 2.025 | Unlike | 1.434 | Unlike | 2.234 | Unlike | 1.434 | Unlike | 2.286 | Unlike | | |
| 21 | 1.5 | 8 | 0.436 | Like | 0.731 | Like | 0.932 | Like | 1.538 | Unlike | 1.800 | Unlike | 0.932 | Like | 1.808 | Unlike | 0.932 | Like | 1.719 | Unlike | | |
| 22 | 6 | 45 | 1.556 | Unlike | 2.171 | Unlike | 2.029 | Unlike | 3.036 | Unlike | 3.819 | Unlike | 2.975 | Unlike | 4.304 | Unlike | 2.975 | Unlike | 4.437 | Unlike | | |
| 23 | 4.5 | 13 | 0.469 | Like | 0.458 | Like | 0.683 | Like | 0.791 | Like | 0.919 | Like | 0.951 | Like | 0.971 | Like | 0.951 | Like | 0.967 | Like | | |
| 24 | 6 | 21 | 0.562 | Like | 0.853 | Like | 0.755 | Like | 1.224 | Unlike | 1.539 | Unlike | 1.14 | Unlike | 1.729 | Unlike | 1.14 | Unlike | 1.783 | Unlike | | |
| 25 | 1.5 | 6 | 0.344 | Like | 0.824 | Like | 0.761 | Like | 1.749 | Unlike | 0.761 | Like | 0.761 | Like | 0.813 | Like | 0.761 | Like | 2.025 | Unlike | | |
| 26 | 3 | 28 | 0.957 | Like | 1.312 | Unlike | 1.83 | Unlike | 2.071 | Unlike | 2.449 | Unlike | 1.83 | Unlike | 2.642 | Unlike | 1.830 | Unlike | 2.656 | Unlike | | |
| 27 | 4.5 | 28 | 0.75 | Like | 1.154 | Unlike | 1.054 | Unlike | 1.703 | Unlike | 2.025 | Unlike | 1.434 | Unlike | 2.234 | Unlike | 1.434 | Unlike | 2.286 | Unlike | | |
| 28 | 6 | 45 | 1.556 | Unlike | 2.171 | Unlike | 2.029 | Unlike | 3.036 | Unlike | 3.819 | Unlike | 2.975 | Unlike | 4.304 | Unlike | 2.975 | Unlike | 4.437 | Unlike | | |
| 29 | 4.5 | 13 | 0.469 | Like | 0.458 | Like | 0.683 | Like | 0.791 | Like | 0.919 | Like | 0.951 | Like | 0.971 | Like | 0.951 | Like | 0.967 | Like | | |
| 30 | 6 | 21 | 0.562 | Like | 0.853 | Like | 0.755 | Like | 1.224 | Unlike | 1.539 | Unlike | 1.14 | Unlike | 1.729 | Unlike | 1.14 | Unlike | 1.783 | Unlike | | |
| 31 | 1.5 | 6 | 0.344 | Like | 0.824 | Like | 0.761 | Like | 1.749 | Unlike | 2.113 | Unlike | 0.761 | Like | 2.134 | Unlike | 0.761 | Like | 2.025 | Unlike | | |
| 32 | 3 | 28 | 0.957 | Like | 1.312 | Unlike | 1.83 | Unlike | 2.071 | Unlike | 2.449 | Unlike | 1.83 | Unlike | 2.642 | Unlike | 1.830 | Unlike | 2.656 | Unlike | | |
| 33 | 4.5 | 28 | 0.75 | Like | 1.154 | Unlike | 1.054 | Unlike | 1.703 | Unlike | 2.025 | Unlike | 1.434 | Unlike | 2.234 | Unlike | 1.434 | Unlike | 2.286 | Unlike | | |
| 34 | 6 | 45 | 1.556 | Unlike | 2.171 | Unlike | 2.029 | Unlike | 3.036 | Unlike | 3.819 | Unlike | 2.975 | Unlike | 4.304 | Unlike | 2.975 | Unlike | 4.437 | Unlike | | |
| 35 | 7.5 | 28 | 0.746 | Like | 0.839 | Like | 0.928 | Like | 0.967 | Like | 1.177 | Unlike | 1.291 | Unlike | 1.417 | Unlike | 1.427 | Unlike | 1.545 | Unlike | | |

Tab. III(b) Liquefaction potential from MLR model for earthquake magnitude 6.0 with varying water level.

| S. No. | Depth (z) | SPT _N value | For network: MFW ₀ | | | For network: MFW ₁ | | | For network: MFW ₂ | | | For network: MFW ₃ | | | For network: MFW ₄ | | | For network: MFW ₅ | | | For network: MFW ₆ | | | | | |
|--------|-----------|------------------------|-------------------------------|-------|--------|-------------------------------|--------|--------|-------------------------------|-------|--------|-------------------------------|--------|--------|-------------------------------|-------|--------|-------------------------------|--------|--------|-------------------------------|-------|--------|----------------------|--------|--------|
| | | | lique. Pot. by I & B method | ratio | status | lique. Pot. by ANFIS | ratio | status | lique. Pot. by I & B method | ratio | status | lique. Pot. by ANFIS | ratio | status | lique. Pot. by I & B method | ratio | status | lique. Pot. by ANFIS | ratio | status | lique. Pot. by I & B method | ratio | status | lique. Pot. by ANFIS | ratio | status |
| 1 | 4.5 | 22 | Like | 0.452 | Like | 0.654 | Like | 0.857 | Like | 0.907 | Like | 0.907 | Like | 0.907 | Like | 0.907 | Like | 0.907 | Like | 0.907 | Like | 0.907 | Like | 0.907 | Like | 0.907 |
| 2 | 6 | 21 | Like | 0.41 | Like | 0.378 | Like | 0.544 | Like | 0.549 | Like | 0.678 | Like | 0.695 | Like | 0.812 | Like | 0.798 | Like | 0.812 | Like | 0.812 | Like | 0.823 | Like | 0.823 |
| ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 8 | 4.5 | 28 | Like | 0.548 | Like | 0.582 | Like | 0.77 | Like | 0.778 | Like | 0.993 | Like | 1.037 | Unlike | 1.048 | Unlike | 1.072 | Unlike | 1.048 | Unlike | 1.048 | Unlike | 1.029 | Unlike | 1.029 |
| ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 33 | 6 | 45 | Unlike | 1.121 | Unlike | 1.134 | Unlike | 1.25 | Unlike | 1.27 | Unlike | 1.25 | Unlike | 1.192 | Unlike | 1.25 | Unlike | 1.249 | Unlike | 1.25 | Unlike | 1.25 | Unlike | 1.25 | Unlike | 1.25 |
| 34 | 7.5 | 28 | Like | 0.529 | Like | 0.464 | Like | 0.658 | Like | 0.594 | Like | 0.787 | Like | 0.691 | Like | 0.916 | Like | 0.82 | Like | 1.013 | Unlike | 0.812 | Like | 0.812 | Like | 0.812 |

Tab. IV(a) Liquefaction potential from ANFIS models for earthquake magnitude 7.0 with varying water level.

| S. No. | Depth (z) | SPT _N value | For network: MFW ₀ | | | For network: MFW ₁ | | | For network: MFW ₂ | | | For network: MFW ₃ | | | For network: MFW ₄ | | | For network: MFW ₅ | | | For network: MFW ₆ | | | | | |
|--------|-----------|------------------------|-------------------------------|-------|--------|-------------------------------|--------|--------|-------------------------------|-------|--------|-------------------------------|--------|--------|-------------------------------|-------|--------|-------------------------------|--------|--------|-------------------------------|-------|--------|--------------------|--------|--------|
| | | | lique. Pot. by I & B method | ratio | status | lique. Pot. by MLR | ratio | status | lique. Pot. by I & B method | ratio | status | lique. Pot. by MLR | ratio | status | lique. Pot. by I & B method | ratio | status | lique. Pot. by MLR | ratio | status | lique. Pot. by I & B method | ratio | status | lique. Pot. by MLR | ratio | status |
| 1 | 4.5 | 22 | Like | 0.452 | Like | 0.824 | Like | 0.654 | Like | 1.316 | Unlike | 0.857 | Like | 1.629 | Unlike | 0.907 | Like | 1.766 | Unlike | 0.907 | Like | 1.766 | Unlike | 0.907 | Like | 1.769 |
| 2 | 6 | 21 | Like | 0.410 | Like | 0.472 | Like | 0.544 | Like | 0.630 | Like | 0.678 | Like | 0.723 | Like | 0.812 | Like | 0.829 | Like | 0.812 | Like | 0.884 | Like | 0.812 | Like | 0.884 |
| ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 8 | 4.5 | 28 | Like | 0.548 | Like | 0.836 | Like | 0.770 | Like | 1.238 | Unlike | 0.993 | Like | 1.471 | Unlike | 1.048 | Unlike | 1.621 | Unlike | 1.048 | Unlike | 1.657 | Unlike | 1.048 | Unlike | 1.657 |
| 9 | 6 | 45 | Unlike | 1.121 | Unlike | 1.563 | Unlike | 1.462 | Unlike | 2.191 | Unlike | 1.803 | Unlike | 2.756 | Unlike | 2.144 | Unlike | 3.104 | Unlike | 2.144 | Unlike | 3.197 | Unlike | 2.144 | Unlike | 3.197 |
| 10 | 4.5 | 13 | Like | 0.343 | Like | 0.336 | Like | 0.499 | Like | 0.582 | Like | 0.656 | Like | 0.676 | Like | 0.695 | Like | 0.713 | Like | 0.695 | Like | 0.710 | Like | 0.695 | Like | 0.710 |
| 11 | 6 | 21 | Like | 0.405 | Like | 0.613 | Like | 0.544 | Like | 0.882 | Like | 0.682 | Like | 1.110 | Unlike | 0.821 | Like | 1.246 | Unlike | 0.821 | Like | 1.284 | Unlike | 0.821 | Like | 1.284 |
| 12 | 1.5 | 6 | Like | 0.258 | Like | 0.625 | Like | 0.571 | Like | 1.313 | Unlike | 0.571 | Like | 1.582 | Unlike | 0.571 | Like | 1.600 | Unlike | 0.571 | Like | 1.524 | Unlike | 0.571 | Like | 1.524 |
| 13 | 6 | 12 | Like | 0.284 | Like | 0.078 | Like | 0.384 | Like | 0.040 | Like | 0.485 | Like | 0.000 | Like | 0.585 | Like | 0.014 | Like | 0.585 | Like | 0.070 | Like | 0.585 | Like | 0.070 |
| 14 | 1.5 | 6 | Like | 0.258 | Like | 0.625 | Like | 0.571 | Like | 1.313 | Unlike | 0.571 | Like | 1.582 | Unlike | 0.571 | Like | 1.600 | Unlike | 0.571 | Like | 1.524 | Unlike | 0.571 | Like | 1.524 |
| ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 18 | 3 | 27 | Like | 0.785 | Like | 1.494 | Unlike | 1.810 | Unlike | 2.428 | Unlike | 1.810 | Unlike | 3.104 | Unlike | 1.810 | Unlike | 3.368 | Unlike | 1.810 | Unlike | 3.368 | Unlike | 1.810 | Unlike | 3.368 |
| 19 | 4.5 | 40 | Unlike | 1.493 | Unlike | 2.020 | Unlike | 2.359 | Unlike | 3.090 | Unlike | 3.226 | Unlike | 4.011 | Unlike | 3.442 | Unlike | 4.429 | Unlike | 3.442 | Unlike | 4.479 | Unlike | 3.442 | Unlike | 4.479 |
| 20 | 6 | 49 | Unlike | 1.389 | Unlike | 2.222 | Unlike | 1.906 | Unlike | 3.280 | Unlike | 2.422 | Unlike | 4.260 | Unlike | 2.939 | Unlike | 4.745 | Unlike | 2.939 | Unlike | 4.824 | Unlike | 2.939 | Unlike | 4.824 |
| 21 | 1.5 | 8 | Like | 0.327 | Like | 0.554 | Like | 0.699 | Like | 1.154 | Unlike | 0.699 | Like | 1.349 | Unlike | 0.699 | Like | 1.358 | Unlike | 0.699 | Like | 1.295 | Unlike | 0.699 | Like | 1.295 |
| ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 26 | 1.5 | 6 | Like | 0.258 | Like | 0.625 | Like | 0.571 | Like | 1.313 | Unlike | 0.571 | Like | 1.582 | Unlike | 0.571 | Like | 1.600 | Unlike | 0.571 | Like | 1.524 | Unlike | 0.571 | Like | 1.524 |
| ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... | ... |
| 32 | 4.5 | 28 | Like | 0.548 | Like | 0.836 | Like | 0.770 | Like | 1.238 | Unlike | 0.993 | Like | 1.471 | Unlike | 1.048 | Unlike | 1.621 | Unlike | 1.048 | Unlike | 1.657 | Unlike | 1.048 | Unlike | 1.657 |
| 33 | 6 | 45 | Unlike | 1.121 | Unlike | 1.563 | Unlike | 1.462 | Unlike | 2.191 | Unlike | 1.803 | Unlike | 2.756 | Unlike | 2.144 | Unlike | 3.104 | Unlike | 2.144 | Unlike | 3.197 | Unlike | 2.144 | Unlike | 3.197 |
| 34 | 7.5 | 28 | Like | 0.529 | Like | 0.591 | Like | 0.658 | Like | 0.678 | Like | 0.787 | Like | 0.827 | Like | 0.916 | Like | 0.997 | Like | 1.013 | Unlike | 0.812 | Like | 1.013 | Unlike | 0.812 |

Tab. IV(b) Liquefaction potential from MLR model for earthquake magnitude 7.0 with varying water level.

| S. No. | Depth (z) | SPT-N value | For network MAW ₀ | | | For network MAW ₁ | | | For network MAW ₂ | | | For network MAW ₃ | | |
|--------|-----------|-------------|------------------------------|--------|--------|------------------------------|-------|--------|------------------------------|-------|--------|------------------------------|-------|--------|
| | | | lique. Pot. by I & B method | ratio | status | lique. Pot. by I & B method | ratio | status | lique. Pot. by I & B method | ratio | status | lique. Pot. by I & B method | ratio | status |
| 1 | 4.5 | 22 | 0.329 | 0.329 | Like | 0.477 | 0.477 | Like | 0.624 | 0.624 | Like | 0.661 | 0.661 | Like |
| 2 | 6 | 21 | 0.295 | 0.2891 | Like | 0.391 | 0.337 | Like | 0.487 | 0.477 | Like | 0.583 | 0.573 | Like |
| 3 | 3 | 28 | 0.523 | 0.427 | Like | 0.981 | 0.968 | Like | 1.001 | 1.061 | Unlike | 1.001 | 1.049 | Unlike |
| 4 | 3 | 27 | 0.58 | 0.485 | Like | 1.336 | 1.104 | Unlike | 1.25 | 1.222 | Unlike | 1.25 | 1.214 | Unlike |
| 5 | 3 | 27 | 0.58 | 0.485 | Like | 1.336 | 1.104 | Unlike | 1.25 | 1.222 | Unlike | 1.25 | 1.214 | Unlike |
| 6 | 7.5 | 28 | 0.374 | 0.2931 | Like | 0.466 | 0.41 | Like | 0.557 | 0.479 | Like | 0.648 | 0.608 | Like |

Tab. V(a) Liquefaction potential from ANFIS models for earthquake magnitude 8.0 with varying water level.

| S. No. | Depth (z) | SPT-N value | For network MAW ₀ | | | For network MAW ₁ | | | For network MAW ₂ | | | For network MAW ₃ | | |
|--------|-----------|-------------|------------------------------|-------|--------|------------------------------|-------|--------|------------------------------|-------|--------|------------------------------|-------|--------|
| | | | lique. Pot. by I & B method | ratio | status | lique. Pot. by I & B method | ratio | status | lique. Pot. by I & B method | ratio | status | lique. Pot. by I & B method | ratio | status |
| 7 | 4.5 | 22 | 0.329 | 0.600 | Like | 0.477 | 0.960 | Like | 0.624 | 1.187 | Unlike | 0.661 | 1.286 | Unlike |
| 8 | 4.5 | 28 | 0.399 | 0.604 | Like | 0.561 | 0.898 | Like | 0.723 | 1.065 | Unlike | 0.764 | 1.172 | Unlike |
| 9 | 6 | 45 | 0.805 | 1.122 | Unlike | 1.050 | 1.576 | Unlike | 1.294 | 1.983 | Unlike | 1.539 | 2.232 | Unlike |
| 10 | 4.5 | 13 | 0.250 | 0.246 | Like | 0.364 | 0.427 | Like | 0.478 | 0.495 | Like | 0.506 | 0.522 | Like |
| 11 | 6 | 21 | 0.291 | 0.440 | Like | 0.390 | 0.634 | Like | 0.490 | 0.798 | Like | 0.590 | 0.895 | Like |
| 12 | 1.5 | 6 | 0.193 | 0.472 | Like | 0.427 | 0.981 | Like | 0.427 | 1.179 | Unlike | 0.427 | 1.195 | Unlike |
| 13 | 6 | 12 | 0.204 | 0.050 | Like | 0.276 | 0.020 | Like | 0.348 | 0.000 | Like | 0.420 | 0.000 | Like |
| 14 | 1.5 | 6 | 0.193 | 0.472 | Like | 0.427 | 0.981 | Like | 0.427 | 1.179 | Unlike | 0.427 | 1.195 | Unlike |
| 15 | 3 | 27 | 0.580 | 1.088 | Unlike | 1.336 | 1.771 | Unlike | 1.336 | 2.262 | Unlike | 1.336 | 2.453 | Unlike |
| 16 | 4.5 | 40 | 1.087 | 1.462 | Unlike | 1.719 | 2.239 | Unlike | 2.350 | 2.906 | Unlike | 2.507 | 3.208 | Unlike |
| 17 | 6 | 49 | 0.997 | 1.603 | Unlike | 1.368 | 2.369 | Unlike | 1.739 | 3.078 | Unlike | 2.110 | 3.427 | Unlike |
| 18 | 1.5 | 8 | 0.245 | 0.418 | Like | 0.522 | 0.863 | Like | 0.522 | 1.007 | Unlike | 0.522 | 1.015 | Unlike |
| 19 | 1.5 | 6 | 0.193 | 0.472 | Like | 0.427 | 0.981 | Like | 0.427 | 1.179 | Unlike | 0.427 | 1.195 | Unlike |
| 20 | 4.5 | 28 | 0.399 | 0.604 | Like | 0.561 | 0.898 | Like | 0.723 | 1.065 | Unlike | 0.764 | 1.172 | Unlike |
| 21 | 6 | 45 | 0.805 | 1.122 | Unlike | 1.050 | 1.576 | Unlike | 1.294 | 1.983 | Unlike | 1.539 | 2.232 | Unlike |
| 22 | 6 | 45 | 0.805 | 1.122 | Unlike | 1.050 | 1.576 | Unlike | 1.294 | 1.983 | Unlike | 1.539 | 2.232 | Unlike |
| 23 | 7.5 | 28 | 0.374 | 0.415 | Like | 0.466 | 0.474 | Like | 0.557 | 0.579 | Like | 0.648 | 0.699 | Like |

Tab. V(b) Liquefaction potential from MLR models for earthquake magnitude 8.0 with varying water level.

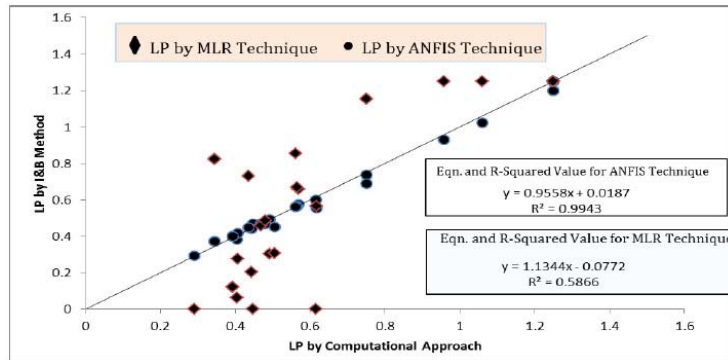


Fig. 3 ANFIS model for *W.T. 0 m and M 6.0*.

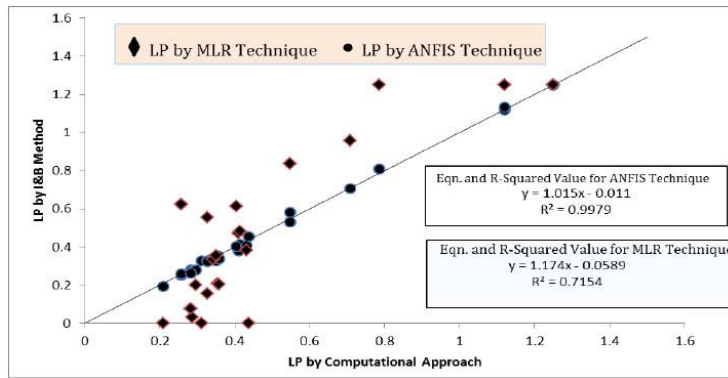


Fig. 4 ANFIS model for *W.T. 0 m and M 7.0*.

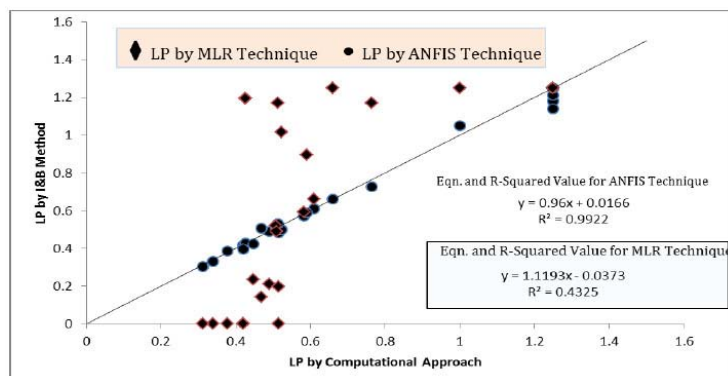


Fig. 5 ANFIS model for *W.T. 6 m and M 8.0*.

datasets, which is within acceptable limit. The comparative study depicts that results obtained from ANFIS models can be used cautiously and performance of models can be upgraded by introducing more sets of data inputs. It can also be observed from Tab. VI that the coefficient of determination obtained from MLR models is in the range of 0.8. In this case mean absolute error and root mean square error is also high. It is also indicative from the above discussion that numbers of incorrect prediction from MLR models is greater than ANFIS models. The comparison of these statistical parameters clearly indicates that COD, MAE and RMSE obtained by ANFIS models are far better than MLR models.

| S. No. | Models | By ANFIS | | | By MLR | | |
|--------|-----------------------------------|--------------|--------------|--------------|---------------|--------------|--------------|
| | | COD | MAE | RMSE | COD | MAE | RMSE |
| 1 | M₆W₀ | 0.995 | 3.140 | 4.490 | 0.852 | 59.93 | 71.47 |
| 2 | M ₆ W ₂ | 0.872 | 6.161 | 9.212 | 0.8475 | 63.09 | 73.09 |
| 3 | M ₆ W ₄ | 0.911 | 6.349 | 8.908 | 0.8274 | 70.49 | 84.77 |
| 4 | M ₆ W ₆ | 0.777 | 8.085 | 10.904 | 0.8338 | 69.76 | 84.54 |
| 5 | M ₆ W ₈ | 0.732 | 8.024 | 11.341 | 0.8380 | 67.38 | 80.65 |
| 6 | M₇W₀ | 0.998 | 2.877 | 3.995 | 0.8515 | 60.80 | 72.58 |
| 7 | M ₇ W ₂ | 0.901 | 5.807 | 8.711 | 0.8455 | 63.52 | 73.56 |
| 8 | M ₇ W ₄ | 0.927 | 5.667 | 8.730 | 0.8265 | 70.59 | 84.82 |
| 9 | M ₇ W ₆ | 0.942 | 4.221 | 6.934 | 0.8334 | 70.09 | 84.85 |
| 10 | M ₇ W ₈ | 0.904 | 5.624 | 9.576 | 0.8378 | 67.85 | 81.18 |
| 11 | M ₈ W ₀ | 0.969 | 2.923 | 5.612 | 0.8514 | 61.55 | 73.51 |
| 12 | M ₈ W ₂ | 0.945 | 4.856 | 6.968 | 0.8433 | 63.94 | 74.05 |
| 13 | M ₈ W ₄ | 0.988 | 2.966 | 5.642 | 0.8254 | 70.70 | 84.86 |
| 14 | M₈W₆ | 0.992 | 2.604 | 3.606 | 0.8330 | 70.35 | 85.08 |
| 15 | M ₈ W ₈ | 0.963 | 4.005 | 7.722 | 0.8376 | 68.24 | 81.58 |

Tab. VI Calculations of coefficient of correlation and average absolute error for each model.

The datasets of one borehole, which was not used in training, and testing of models were used for validation of these models in the end to check the ability of the models if these models are likely to be adopted for prediction of liquefaction potential. The result obtained by conventional I&B method was compared with the predicted condition of liquefaction in like/unlike terms as shown in Tab. VII. This comparison indicates that prediction capability of ANFIS model with high coefficient of determination is in better agreement with the conventional approach in comparison to MLR models.

6. Conclusions

Estimation of liquefaction potential by soft computing and regression methods using SPT data can be advantageous over the conventional approach. Therefore, ANFIS & MLR models were developed to predict liquefaction potential for a site or region. The results of liquefaction potential obtained in like/unlike form for

| Depth meter | SPT-N Value | Soil Description | Classification | Particle Size Distribution | | | Natural Moisture Content % | Bulk Unit Weight gm/cc | Specific Gravity | Angle of Internal Friction ϕ | LP by I & B Method | LP Prediction by ANFIS Model | LP Prediction by MLR Model |
|----------------|-------------|------------------------------------|----------------|----------------------------|-------|-------|-------------------------------------|------------------------------|------------------|--|--------------------------|---------------------------------------|-------------------------------------|
| | | | | 2.0 | 0.075 | 0.002 | | | | | | | |
| 1.5 | 6 | Non Plastic Silty Soil with Gravel | ML | 90.44 | 81.6 | 3.67 | 32.30 | 1.74 | 2.67 | 20 | Like | Like | Unlike |
| 3.0 | 5 | Non Plastic Silty sand | SM | 99.07 | 46.36 | 0.00 | 25.76 | 1.9 | 2.65 | 20 | Like | Like | Like |
| 4.5 | 12 | Non Plastic Silty sand | SM | 99.07 | 46.36 | 0.00 | 25.76 | 1.9 | 2.65 | 20 | Like | Like | Like |
| 6.0 | 12 | Non Plastic Silty sand | SM | 99.07 | 46.36 | 0.00 | 25.76 | 1.9 | 2.65 | 20 | Like | Like | Like |
| 7.5 | 17 | Non Plastic Silty sand | SM | 99.07 | 46.36 | 0.00 | 25.76 | 1.9 | 2.65 | 20 | Like | Like | Like |
| 9.0 | 23 | Non Plastic Silty sand | SM | 99.07 | 46.36 | 0.00 | 25.76 | 1.9 | 2.65 | 20 | Like | Like | Like |

Tab. VII The comparison depicts that ANFIS model & MLR Technique can predict the LP after proper training and testing.

| Combination | Developed Multi-Linear Equation |
|-------------|--|
| 0.35;6;0 | $= 2.281494 - (0.10516 d) + (0.069095 N) + (0.006684 D_x) + (0.021259 w_f) - (1.6931 \rho_f)$ |
| 0.35;7;0 | $= 1.698935 - (0.08183 d) + (0.049976 N) + (0.005053 D_x) + (0.015554 w_f) - (1.24449 \rho_f)$ |
| 0.35;8;0 | $= 1.259794 - (0.06314 d) + (0.036033 N) + (0.003799 D_x) + (0.011341 w_f) - (0.91134 \rho_f)$ |
| 0.35;6;2 | $= 4.410201 - (0.24532 d) + (0.100098 N) + (0.013324 D_x) + (0.035717 w_f) - (2.95095 \rho_f)$ |
| 0.35;7;2 | $= 3.266915 - (0.18662 d) + (0.072495 N) + (0.009962 D_x) + (0.026115 w_f) - (2.16428 \rho_f)$ |
| 0.35;8;2 | $= 2.410765 - (0.1412 d) + (0.052338 N) + (0.007413 D_x) + (0.019029 w_f) - (1.5816 \rho_f)$ |
| 0.35;6;4 | $= 5.941853 - (0.2828 d) + (0.130454 N) + (0.018231 D_x) + (0.049365 w_f) - (4.17785 \rho_f)$ |
| 0.35;7;4 | $= 4.390949 - (0.2148 d) + (0.094525 N) + (0.013583 D_x) + (0.036071 w_f) - (3.06187 \rho_f)$ |
| 0.35;8;4 | $= 3.232732 - (0.16227 d) + (0.068275 N) + (0.010076 D_x) + (0.026268 w_f) - (2.23602 \rho_f)$ |
| 0.35;6;6 | $= 6.255334 - (0.27224 d) + (0.145815 N) + (0.018823 D_x) + (0.054184 w_f) - (4.52546 \rho_f)$ |
| 0.35;7;6 | $= 4.624643 - (0.20787 d) + (0.105596 N) + (0.014052 D_x) + (0.039575 w_f) - (3.31681 \rho_f)$ |
| 0.35;8;6 | $= 3.406151 - (0.15777 d) + (0.076229 N) + (0.010442 D_x) + (0.028807 w_f) - (2.42232 \rho_f)$ |
| 0.35;6;8 | $= 6.050938 - (0.24685 d) + (0.148326 N) + (0.017493 D_x) + (0.054252 w_f) - (4.43984 \rho_f)$ |
| 0.35;7;8 | $= 4.480592 - (0.19007 d) + (0.107361 N) + (0.013118 D_x) + (0.039626 w_f) - (3.25637 \rho_f)$ |
| 0.35;8;8 | $= 3.304963 - (0.14533 d) + (0.077465 N) + (0.009789 D_x) + (0.028845 w_f) - (2.37979 \rho_f)$ |

Tab. VIII Multi-varied linear equation.

different combination of water table and earthquake magnitude demonstrate the closeness of ANFIS models to I & B method. Thirty-four datasets were used for predicting liquefaction potential for fifteen models which form 510 validated results. Out of 510 predictions, only 12 predictions by ANFIS models deviated from the correct prediction which supports the prediction capabilities of ANFIS models. In this, 98% of predictions are analogous. The mean absolute error varies from 2.604% to 8.085%; root mean square error varies from 3.61 to 11.34% whereas coefficients of determination obtained by these models are more than 0.9 except for a few models. On the other hand MLR, models gave more than 20 incorrect results with high mean absolute error and root mean square error. Based on ANFIS prediction capability ANFIS modeling technique to predict liquefaction potential of soils can be adopted in comparison to MLR models. The analysis of results evidently demonstrates that these ANFIS models can be used effectively and it is more reliable since developed models predicts liquefaction potential correctly for one bore log case.

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